

Tutorial lecture on Modeling and simulation of high-speed interconnects: approaches, challenges, and solutions

Original

Tutorial lecture on Modeling and simulation of high-speed interconnects: approaches, challenges, and solutions / GRIVET TALOCIA, Stefano; Triverio, Piero. - ELETTRONICO. - (2010). (Intervento presentato al convegno 14th IEEE Workshop on Signal Propagation on Interconnects tenutosi a Hildesheim (Germany) nel May 9-12, 2010).

Availability:

This version is available at: 11583/2481392 since: 2015-07-15T07:18:53Z

Publisher:

Published

DOI:

Terms of use:

openAccess

This article is made available under terms and conditions as specified in the corresponding bibliographic description in the repository

Publisher copyright

(Article begins on next page)

Modeling and Simulation of High-Speed Interconnects: Approaches, Challenges and Solutions



Stefano Grivet Talocia, Piero Triverio

Dept. Electronics, Politecnico di Torino

stefano.grivet@polito.it

piero.triverio@polito.it

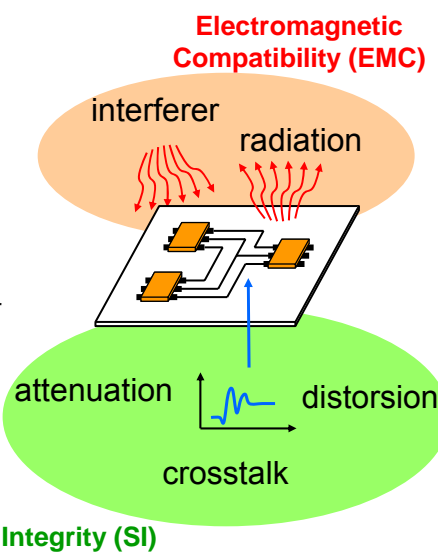
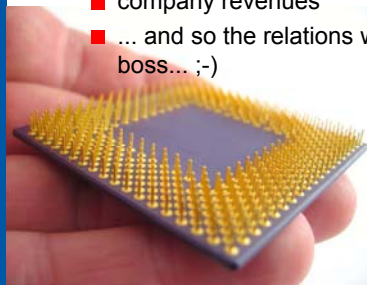
14th IEEE Workshop on Signal Propagation on Interconnects
9 – 12 May 2010, Hildesheim, Germany

Complexity of electronic interconnects

Computer aided design techniques
are essential for interconnects
design.

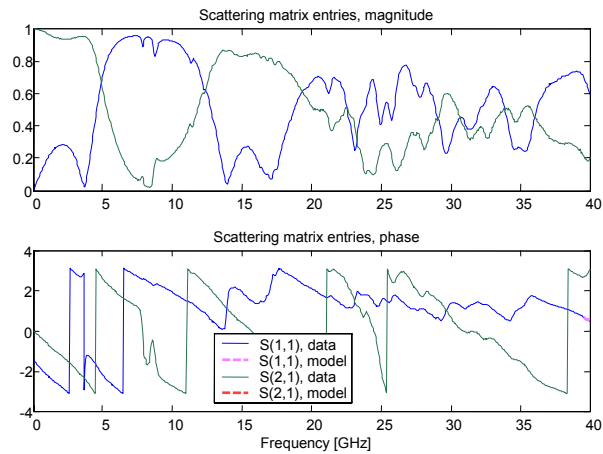
Strong impact on:

- performance & reliability
- product time-to-market
- company revenues
- ... and so the relations with your boss... ;-)



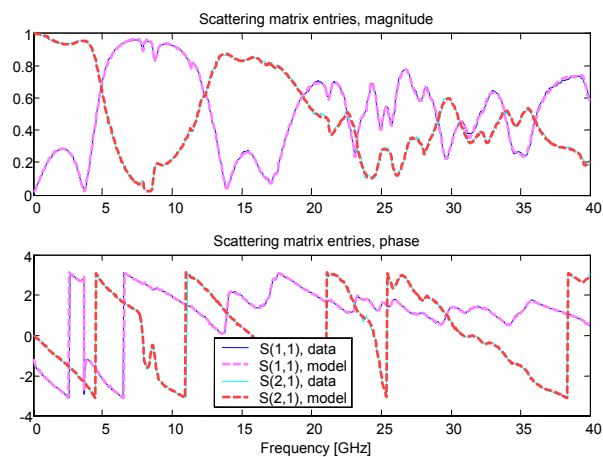
A successful example... (stripline with launches)

Data: measured S-parameters



A successful example... (stripline with launches)

Macromodel: 60 poles

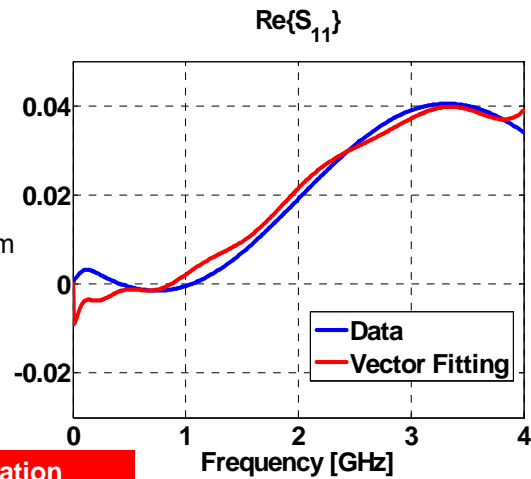


An example of failure... (courtesy of Nokia)

Three coupled lines



Scattering parameters from
an electromagnetic
simulation



**Macromodel generation
dramatically fails! But why?
Where is the problem?**



Computer Aided Design: always hassle-free?

Problems are not uncommon!

Examples:

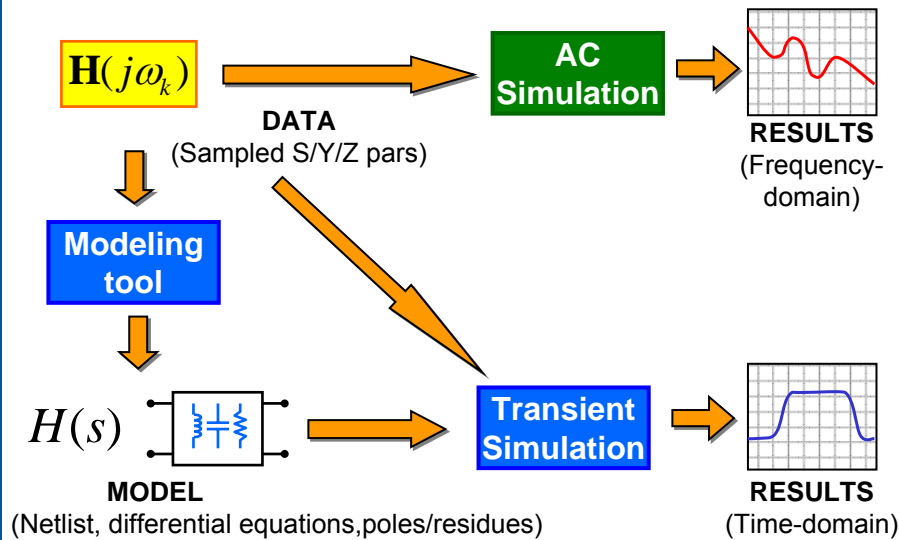
- Simulator errors and warnings ("Convergence failure", "Timestep too small", "Malformed impulse response",...)
- Data fitting problems
- Inaccurate simulation results

Such issues may strongly impair the design workflow!

- Increase product time-to-market
- Post-sale malfunctioning
- Trade performance for reliability

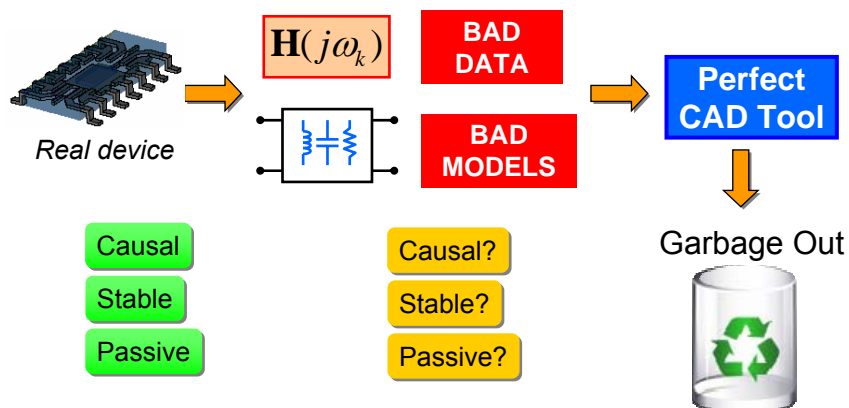


Reference scenario: interconnects simulation



Poor physical consistency is the cause!

A primary cause of these problems is a lack of physical consistency:



Our goal



UNDERSTAND

What do these terms mean!



HOW

Violations can arise



ISSUES

How badly they can ruin my design



BEST PRACTICES

Rules to defeat them

Benefits

Actually, **let us make them work for us**, to improve our design workflow!

■ Measurement step

- Promptly detect inconsistencies & fix the measurement
- ... before wasting hours/days in trying to get the design done!

■ Modeling step

- prevent modeling failures
- maximize accuracy

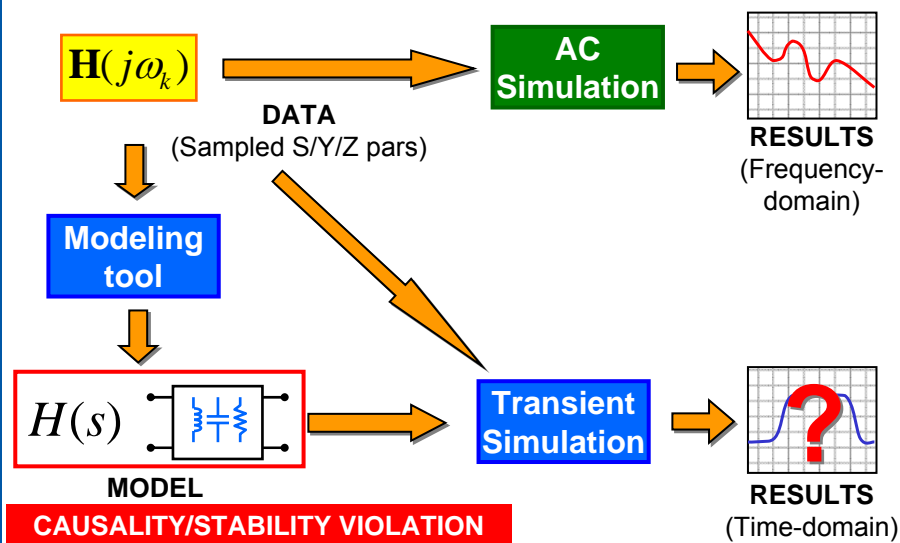
■ Simulation step

- more accurate results
- avoid convergence issues

Agenda

- **Causality & stability of models**
- Causality & stability of frequency data
- Passivity of models
- Passivity of frequency data

Causality/stability violation in a MODEL



Causality: definition

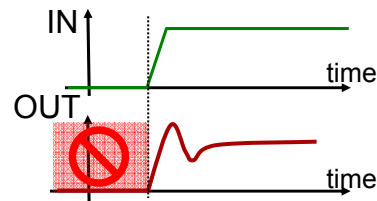
- We consider a linear system (single input single output)

$$w(t) = \int_{-\infty}^{+\infty} h(\tau)x(t-\tau)d\tau$$

$\xrightarrow[\text{IN}]{x(t)}$
 $h(t)$
 $\xrightarrow[\text{OUT}]{w(t)}$

- Causality: “no output before the input”

- No anticipatory behavior
- All physical (real) systems are causal! (active, passive, nonlinear,...)



Causality: definition

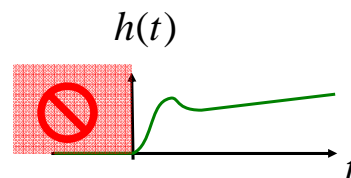
- We consider a linear system (single input single output)

$$w(t) = \int_{-\infty}^{+\infty} h(\tau)x(t-\tau)d\tau$$

$\xrightarrow[\text{IN}]{x(t)}$
 $h(t)$
 $\xrightarrow[\text{OUT}]{w(t)}$

- Causal system:

$h(t) = 0 \quad t < 0$



NONCAUSAL ZONE
CAUSAL ZONE

Stability: definition

- BIBO Stability: “if any Bounded Input leads to a Bounded Output”

$$w(t) = \int_{-\infty}^{+\infty} h(\tau)x(t-\tau)d\tau \quad \xrightarrow[\text{IN } x(t)]{\quad} \boxed{h(t)} \quad \xrightarrow[\text{OUT } w(t)]{\quad}$$

- Stability condition:

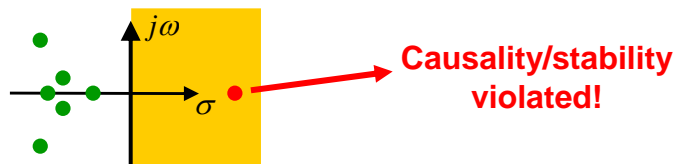
$$\int_{-\infty}^{+\infty} |h(t)|dt < \infty$$

Causality and stability in Laplace domain

- We apply the Laplace transform

$$w(t) = \int_{-\infty}^{+\infty} h(\tau)x(t-\tau)d\tau \quad \xrightarrow{L} \quad W(s) = H(s)X(s)$$

- Causality & stability condition (for lumped systems):
if all poles of $H(s)$ lie in the left hand plane $\text{Re}\{s\} < 0$,
then the system is stable and causal



Causality/stability violations in MODELS



HOW can causality/stability violations arise?

- Causality/stability not enforced by modeling algorithm
- Noisy data
- Model order too large (estimation of redundant poles ill-conditioned)
- What happens when a model is not causal/stable?

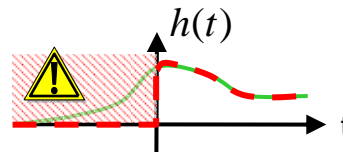


Causality/stability violations in MODELS: issues



Many commonly used theoretical results may be inappropriate! Example: Laplace transform

$$H(s) = \int_0^{+\infty} h(t) e^{-st} dt$$



- The commonly used **one-sided** Laplace transform is not appropriate for possibly non-causal systems!
- Two-sided Laplace transform must be used!

$$H(s) = \int_{-\infty}^{+\infty} h(t) e^{-st} dt$$

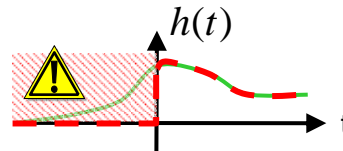
- More complicated.... here avoided!



Causality/stability violations in MODELS: issues

Another example: which convolution formula?

$$w(t) = \int\limits_{\boxed{0}}^{\boxed{t}} h(\tau)x(t-\tau)d\tau$$



- OK only for causal systems! Otherwise integration must be performed from $-\infty$ to $+\infty$



Time-domain circuit simulators based on the convolution formula may not support noncausal models!



Causality/stability violations in MODELS: issues

We consider those simulators that directly integrate the circuit differential equations:

$$\boxed{H(s)} \Rightarrow \dot{\mathbf{y}}(t) = \mathbf{A}\mathbf{y}(t) + \mathbf{B}x(t)$$

$$\mathbf{y}(0) = ?$$

Initial condition



Causality/stability violations in MODELS: issues

We consider those simulators that directly integrate the circuit differential equations:

$$H(s)$$

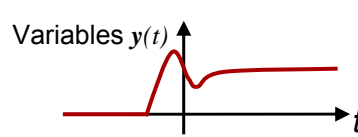
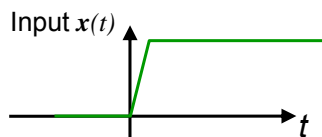


$$\dot{\mathbf{y}}(t) = \mathbf{A}\mathbf{y}(t) + \mathbf{B}x(t)$$

$$\mathbf{y}(0) = 0$$

Initial condition

Wrong for non-causal models!!



Time-domain simulators based on integration of differential equations **do not support noncausal models!**

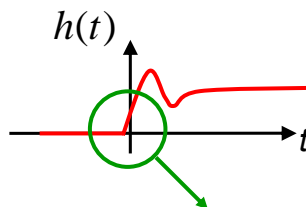


Causality/stability violations in MODELS: issues



Since all physical systems are causal, a non-causal model is for sure an approximation of the original system

$$H(s)$$



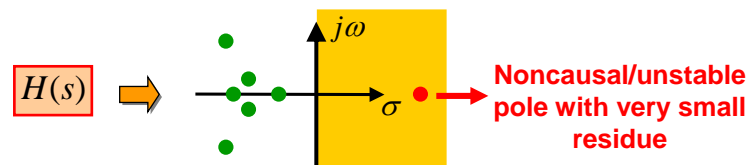
Maybe a good approximation (small causality violation), but...



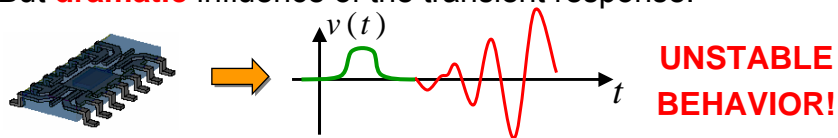
Causality/stability violations in MODELS: issues



Small causality violations can lead to large problems and inconsistencies!



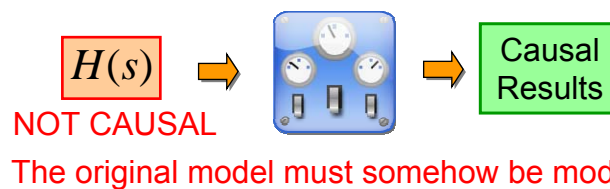
- Negligible effect on the model transfer function $H(s)$
- But **dramatic** influence of the transient response!



Best practices

Bottom line: Noncausal/unstable models can lead to serious problems!

- Always enforce stability and causality during model construction (with any method):
 - Vector Fitting **OK**
 - Many order reduction methods **OK**
- Safer than enforcing causality during circuit simulation





Best practices

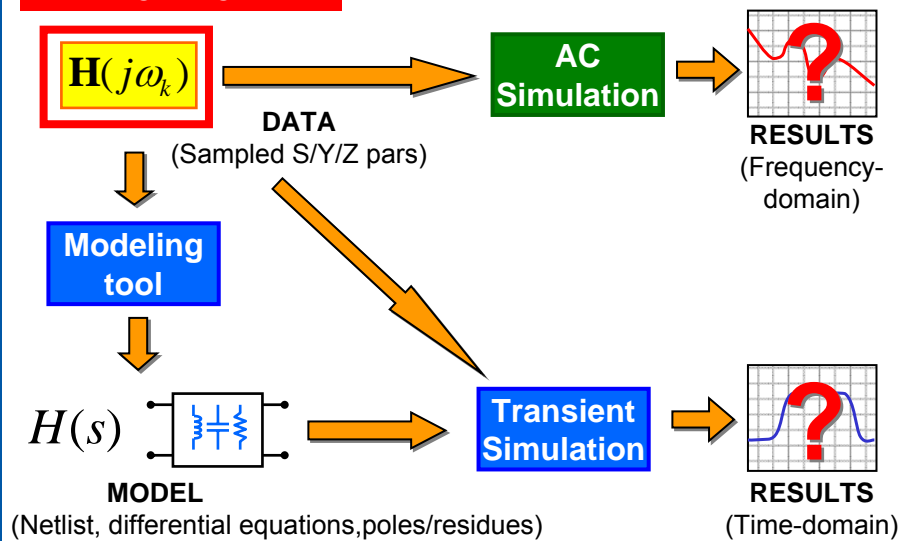
Bottom line: Noncausal/unstable models can lead to serious problems!

- Always enforce stability and causality during model construction (with any method):
 - Vector Fitting **OK**
 - Many order reduction methods **OK**
- Safer than enforcing causality during circuit simulation



CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA



Causality in frequency domain

- We apply the Fourier transform

$$w(t) = \int_{-\infty}^{+\infty} h(\tau)x(t-\tau)d\tau \xrightarrow{F} W(j\omega) = H(j\omega)X(j\omega)$$

- This is mathematically correct only for **stable** systems
- Causality condition: the frequency response must satisfy the **Kramers-Krönig dispersion relations** (Hilbert transform)

$$H(j\omega) = U(\omega) + jV(\omega)$$



$$\begin{cases} U(\omega) = \frac{1}{\pi} p.v. \int_{-\infty}^{+\infty} V(\omega') \frac{d\omega'}{\omega - \omega'} \\ V(\omega) = -\frac{1}{\pi} p.v. \int_{-\infty}^{+\infty} U(\omega') \frac{d\omega'}{\omega - \omega'} \end{cases}$$



Causality violations in FREQUENCY DATA



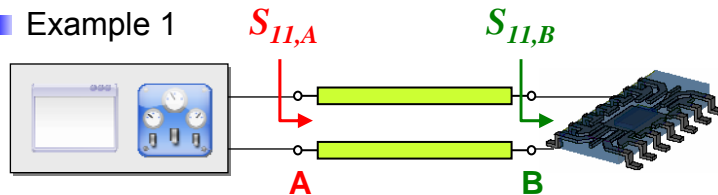
HOW can causality violations arise?

- **Numerical simulation**: poor meshing, bad models or assumptions on material properties, inaccurate solver, human mistakes
- **Measurement**: Improper VNA calibration/de-embedding, human mistake, noise

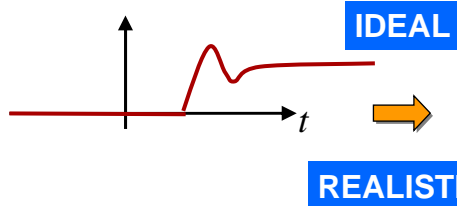


Improper VNA calibration leading to causality violations

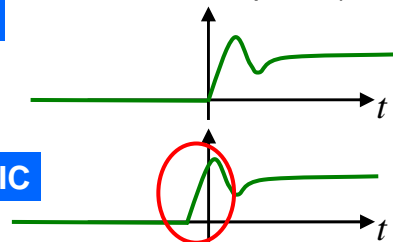
Example 1



Measurement in A:

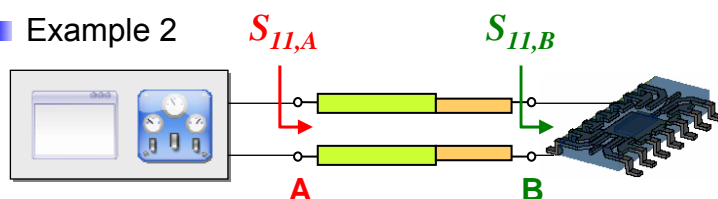


At real device ports (in B):

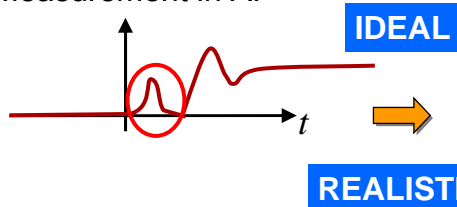


Improper VNA calibration leading to causality violations

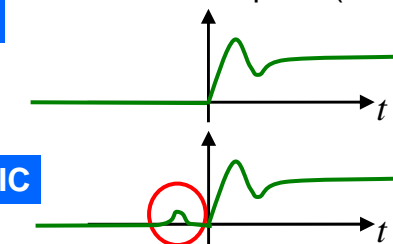
Example 2



Measurement in A:

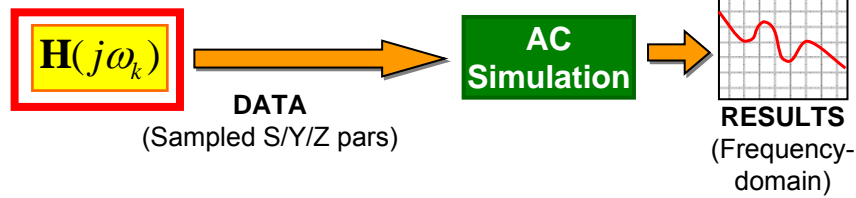


At real device ports (in B):

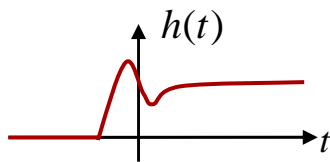


CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA



If transformed to the time-domain:

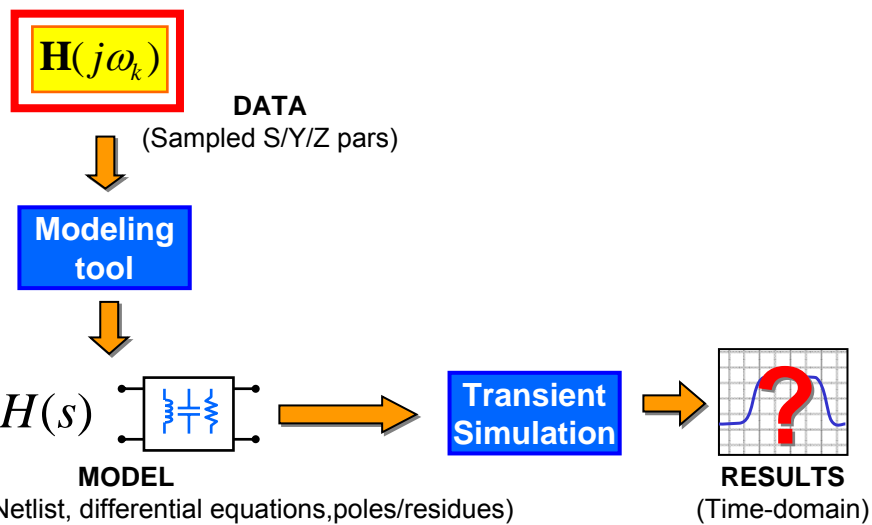


**Non-physical
(non-causal)
results**



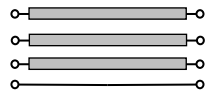
CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA



Example (courtesy of Nokia)

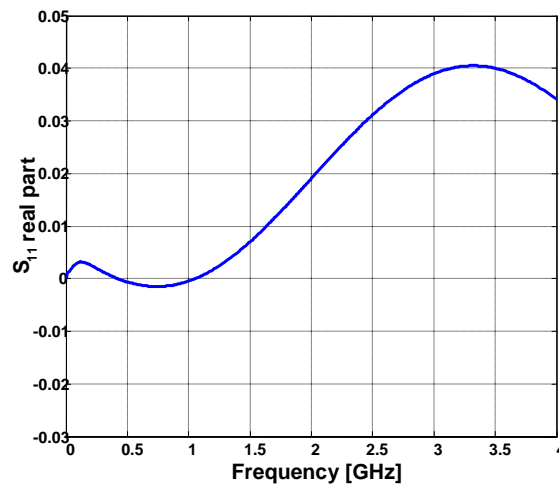
Three coupled lines



EM
simulation

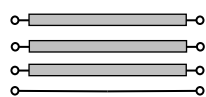
$H(j\omega_k)$

NON-CAUSAL



Example (courtesy of Nokia)

Three coupled lines



EM
simulation

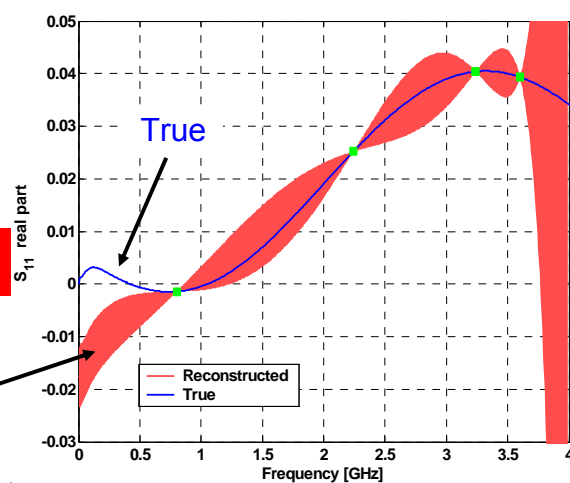
$H(j\omega_k)$

NON-CAUSAL

Computed with
dispersion relations

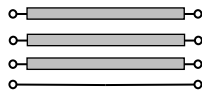


$$H(j\omega) = U(\omega) + jV(\omega)$$

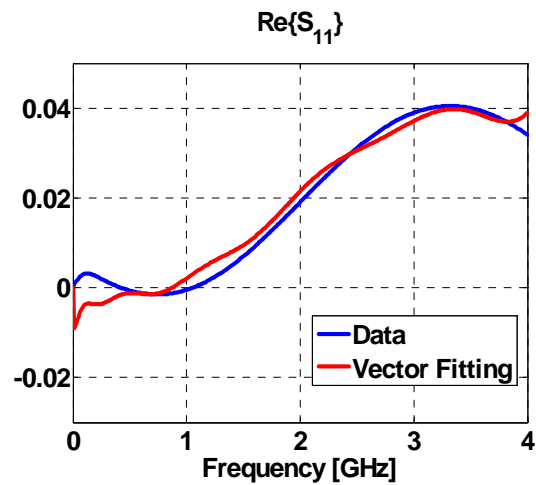


Example (courtesy of Nokia)

Three coupled lines

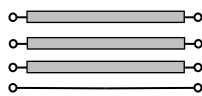


Vector fitting fails...
because of
causality violations!



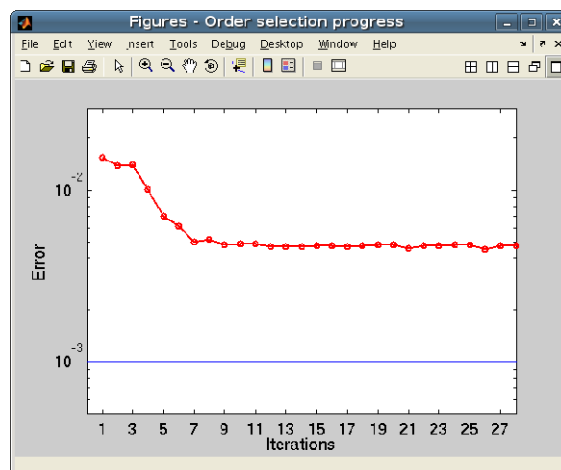
Example (courtesy of Nokia)

Three coupled lines



Vector fitting fails...
because of
causality violations!

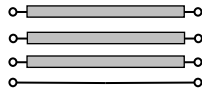
Even if the number
of poles is increased
up to 50, error does
not decrease!



Courtesy of IdemWorks s.r.l.

Example (courtesy of Nokia)

Three coupled lines



**Vector fitting fails...
because of
causality violations!**

```
Building model New using FDVF
Performing FDVF Model Generation ...
Iteration 1
Warning: flipped real pole
Warning: flipped real pole
Warning: flipped real pole
Warning: flipped real pole
RMS Error: 0.00498987 Max Dev: 0.0122055
.... [snip] ....

Iteration 15
Warning: flipped real pole
Warning: flipped real pole
Warning: flipped real pole
Warning: flipped real pole
RMS Error: 0.00385667 Max Dev: 0.0100463
```



Explanation of Vector Fitting difficulties

Vector fitting is required to fulfill two requirements:

■ Accuracy

■ Causality

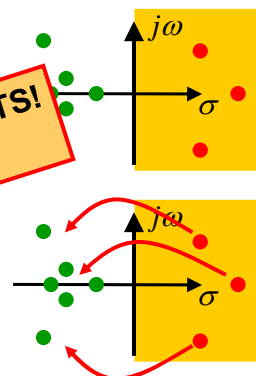
$H(j\omega_k)$



$H(s)$

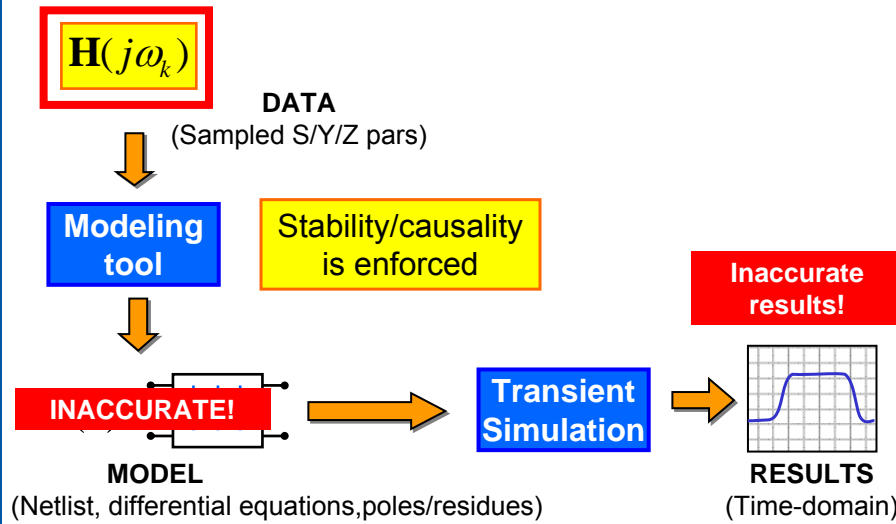
NON CAUSAL
DATA

**CONFLICTING REQUIREMENTS!
NO SOLUTION!**



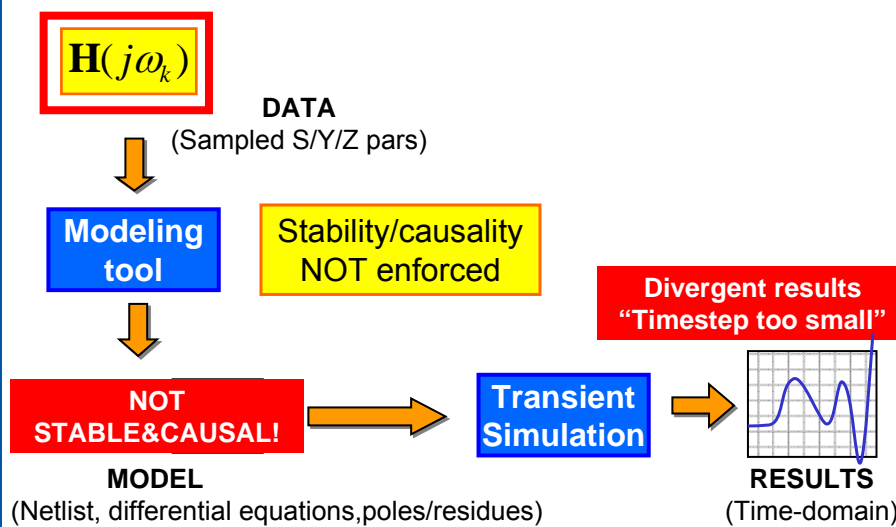
CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA



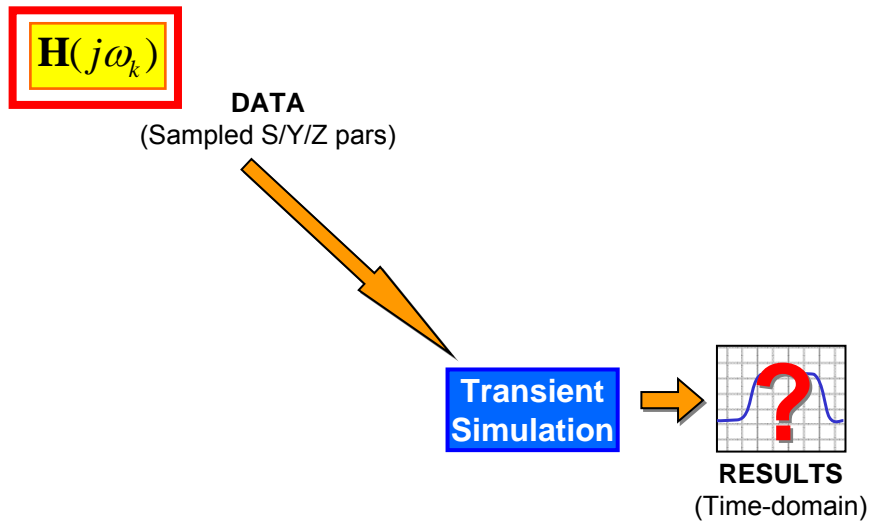
CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA



CAUSALITY/STABILITY VIOLATION

Causality/stability violation in DATA

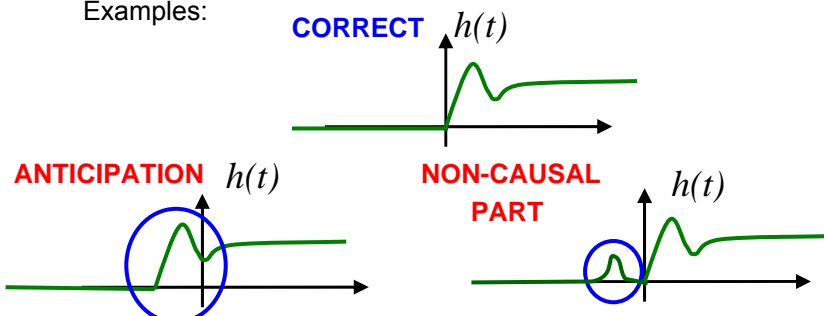


Causality/stability violation in DATA

The simulator must convert the frequency data to the time-domain. It will either:

- fit a macromodel → convergence or accuracy issues
- find the impulse response $h(t)$ and then do convolution → the impulse response will be non-causal

Examples:



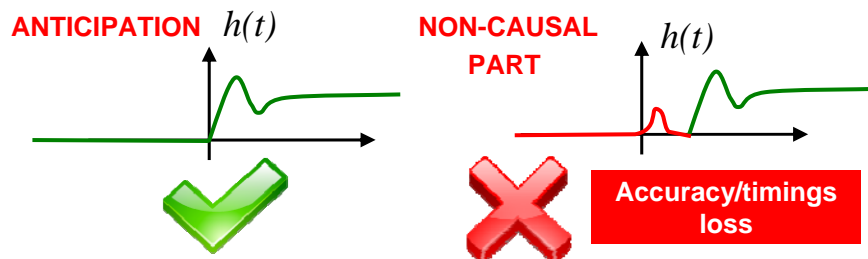
Dealing with a non-causal impulse response

The simulator may:

- do nothing → non-causal waveforms

Will you trust your results?
(may be critical for timing analysis)

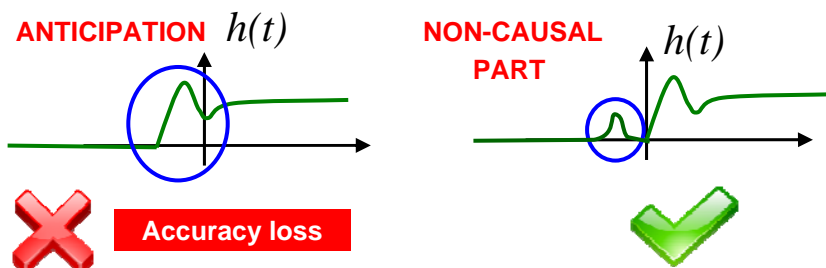
- try to compensate the violation introducing a delay



Dealing with a non-causal impulse response

The simulator may:

- eliminate the non-causal part



Hard to devise a causality-correction method that works well in all cases!

Causal frequency data → avoid any problem!

Causality/stability violation in DATA: conclusion

- Frequency data with causality/stability violations lead to a DEAD END!
- Simulation stability or accuracy is compromised!



Best practices

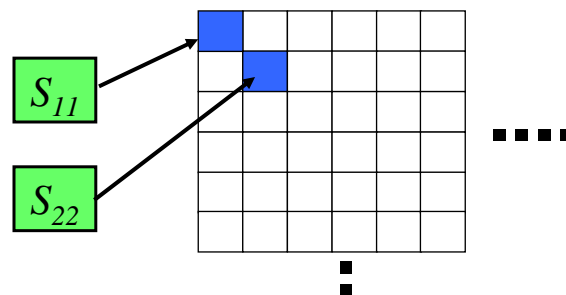
- Check your frequency data for causality violations
- Robust, fully-automated algorithms exist! See [1]
- Reject “bad” datasets and avoid wasting hours trying to get “good” results from them!
- Opportunity to improve your measurement or full-wave simulation process!

[1] P. Triverio and S. Grivet-Talocia, “Robust Causality Characterization via Generalized Dispersion Relations”, IEEE Transactions on Advanced Packaging, vol. 31, n.3, 2008

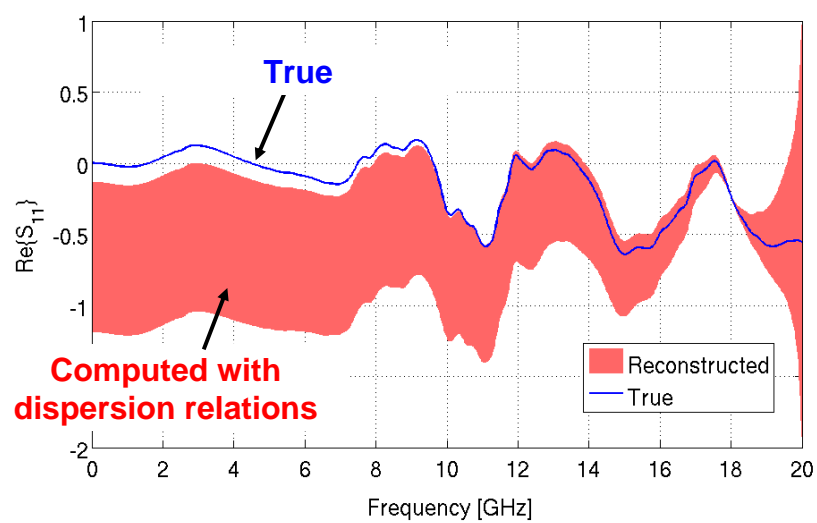
Another example: high-speed connector (courtesy of IBM)

- High performance connector
- Nine signal lines (18 ports)
- Scattering parameters computed with a field solver

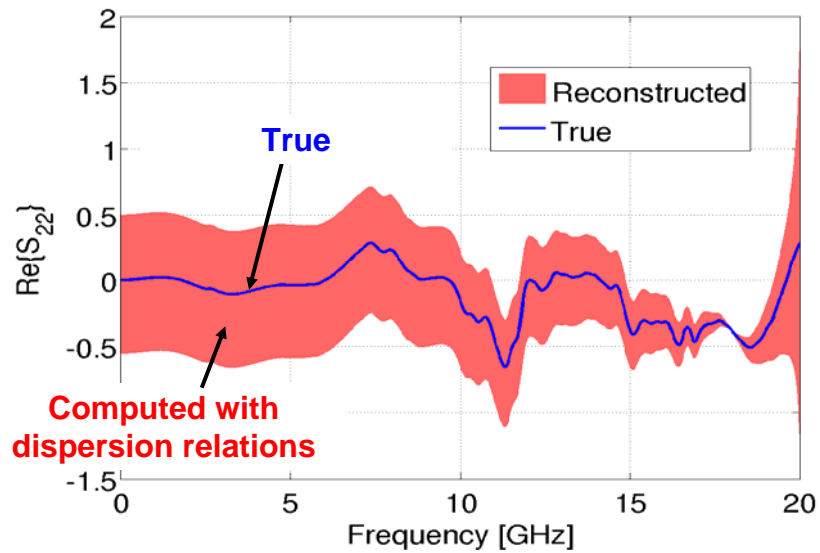
Scattering matrix



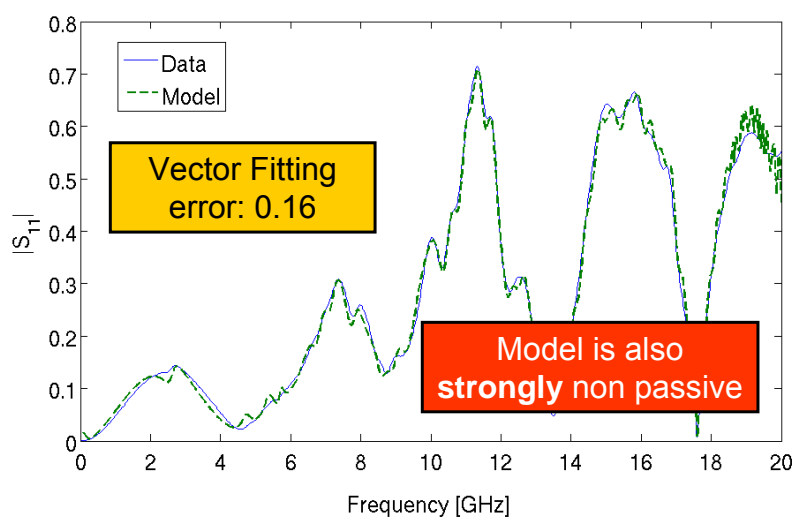
S_{11} is not causal!



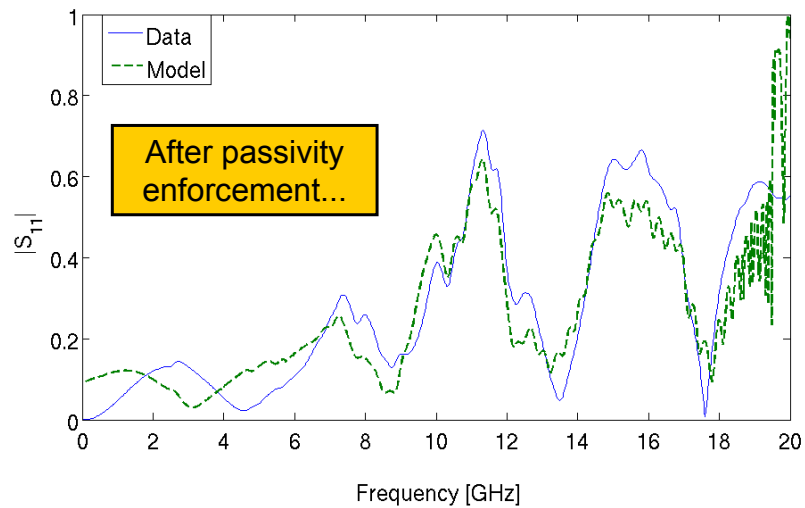
S_{22} is instead consistent



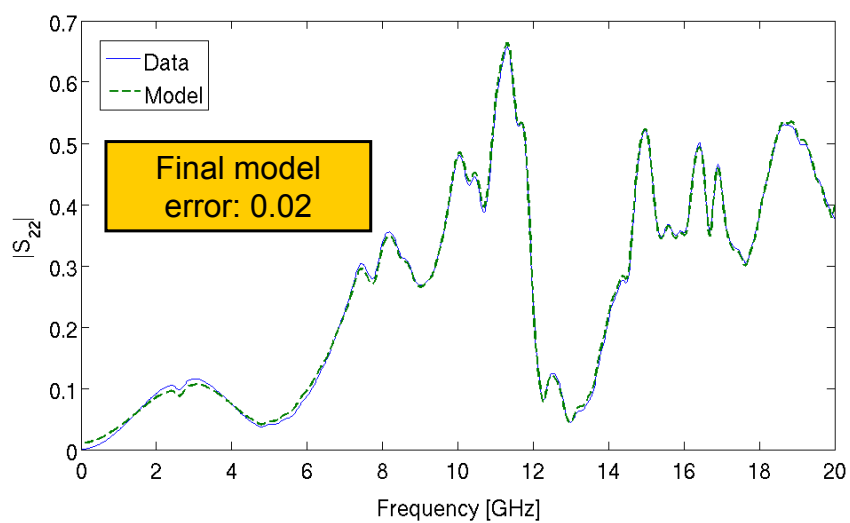
S_{11} modeling is problematic...



S_{11} modeling is very problematic!



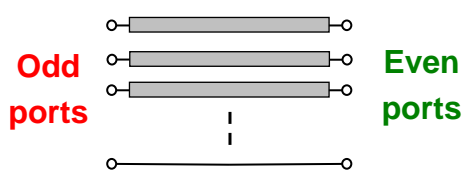
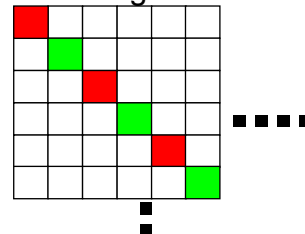
S_{22} modeling instead ends successfully!



Causality violations pattern

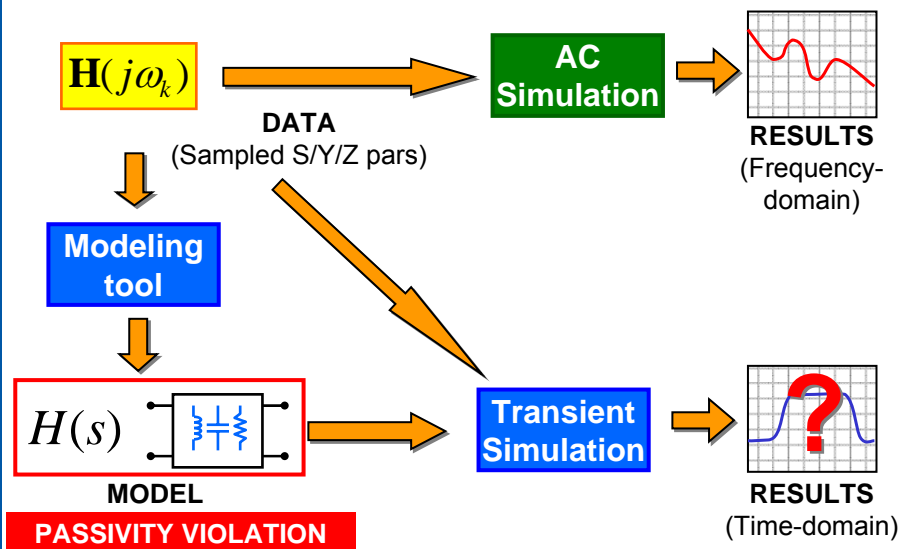
- S_{11} S_{33} S_{55}, \dots violate causality
- S_{22} S_{44} S_{66}, \dots are instead OK

Scattering matrix



- Something got wrong in the de-embedding of odd numbered ports
- Useful information to correct the S-parameters computation!

Passivity violation in a MODEL



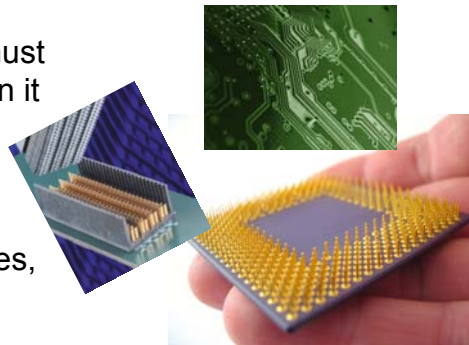
Passivity: definition

- We consider a linear system (with N ports)

$$\mathbf{w}(t) = \int_{-\infty}^{+\infty} \mathbf{h}(\tau) \mathbf{x}(t - \tau) d\tau \quad \xrightarrow[\mathbf{x}(t)]{\text{IN}} \boxed{\mathbf{h}(t)} \xrightarrow[\mathbf{w}(t)]{\text{OUT}}$$

- Passivity: “the system must absorb more energy than it generates”

- True for all interconnect elements (packages, lines, connectors,...)



Passivity conditions for transfer functions

$$\xrightarrow[\mathbf{X}(s)]{\text{IN}} \boxed{\mathbf{H}(s)} \xrightarrow[\mathbf{W}(s)]{\text{OUT}}$$

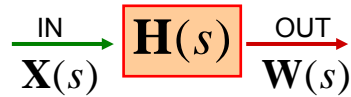
- Scattering representation (similar conclusions for Z/Y)
- Theorem: $\mathbf{H}(s)$ must be **bounded real**, that is:

$$1. \quad \mathbf{H}(s^*) = \mathbf{H}^*(s)$$

To ensure a real-valued $\mathbf{h}(t)$



Passivity conditions for transfer functions

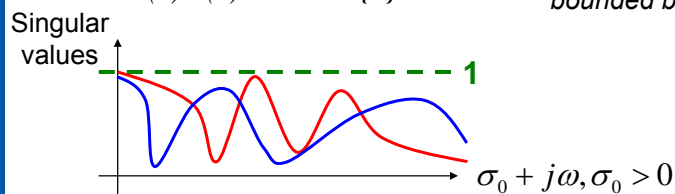


- Scattering representation (similar conclusions for Z/Y)
- Theorem: $\mathbf{H}(s)$ must be **bounded real**, that is:

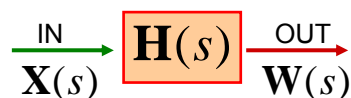
1. $\mathbf{H}(s^*) = \mathbf{H}^*(s)$

2. $\mathbf{H}^H(s)\mathbf{H}(s) \leq \mathbf{I}$ in $\text{Re}\{s\} > 0$

*Singular values of S matrix
bounded by 1 in $\text{Re}\{s\} > 0$*



Passivity conditions for transfer functions



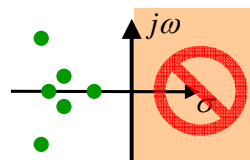
- Scattering representation (similar conclusions for Z/Y)
- Theorem: $\mathbf{H}(s)$ must be **bounded real**, that is:

1. $\mathbf{H}(s^*) = \mathbf{H}^*(s)$

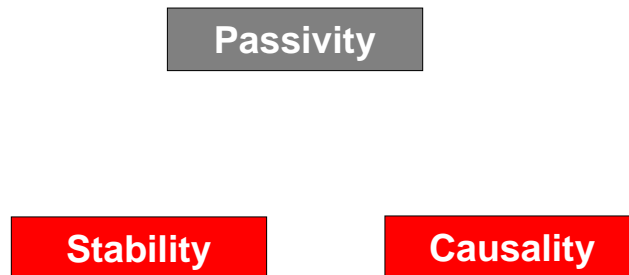
2. $\mathbf{H}^H(s)\mathbf{H}(s) \leq \mathbf{I}$ in $\text{Re}\{s\} > 0$

3. each element of $\mathbf{H}(s)$ be analytic in $\text{Re}\{s\} > 0$

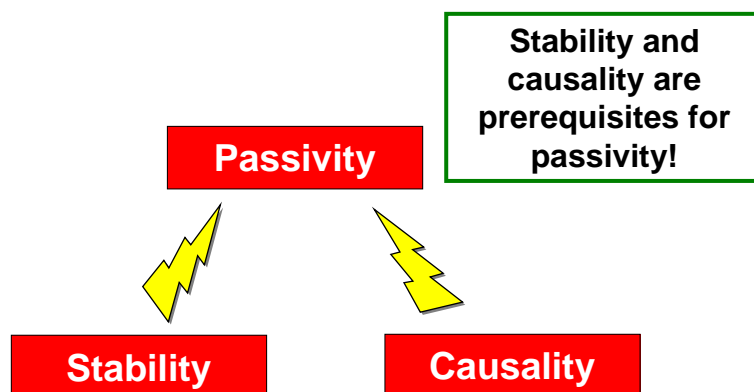
*For lumped systems, no poles
in right half plane*



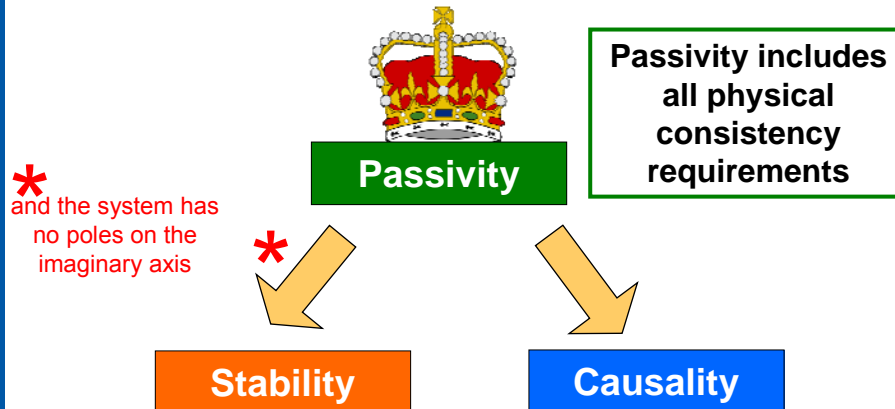
Relation to stability and causality



Relation to stability and causality



Relation to stability and causality



Triverio, Grivet-Talocia, Nakhla, Canavero, Achar, "Stability, causality, and passivity in electrical interconnect models," *IEEE Trans. on Adv. Pack.*, vol. 30, n. 4, Nov. 2007.



Application: passivity violations in MODELS

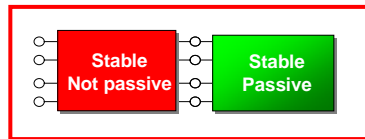


HOW can passivity violations arise?

- Passivity not enforced by modeling algorithm
- Approximation errors
- Common problem, especially for components with low losses (e.g. short interconnects, integrated inductors/capacitors,...)
- What happens if a model is not passive??



Passivity violations in MODELS: issues

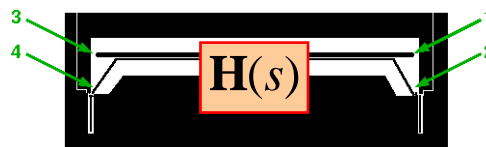


Neither passivity nor stability are guaranteed!



A **non passive** model, connected to **passive** loads may lead to an **unstable** circuit!

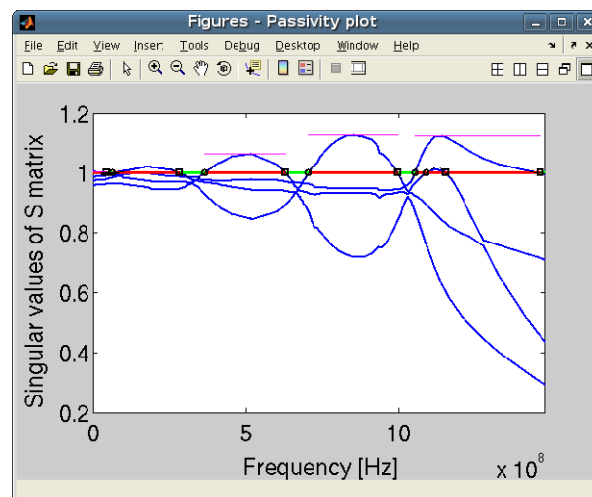
Example:



Not passive



Passivity violations in MODELS: issues

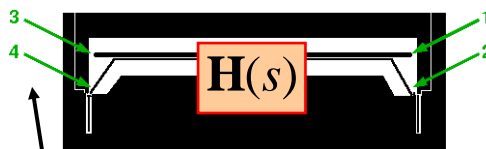


Courtesy of IdemWorks s.r.l.



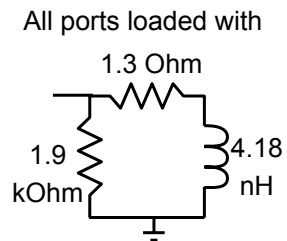
Destabilizing load

- We can always find a passive load that makes the whole system unstable!



Not passive

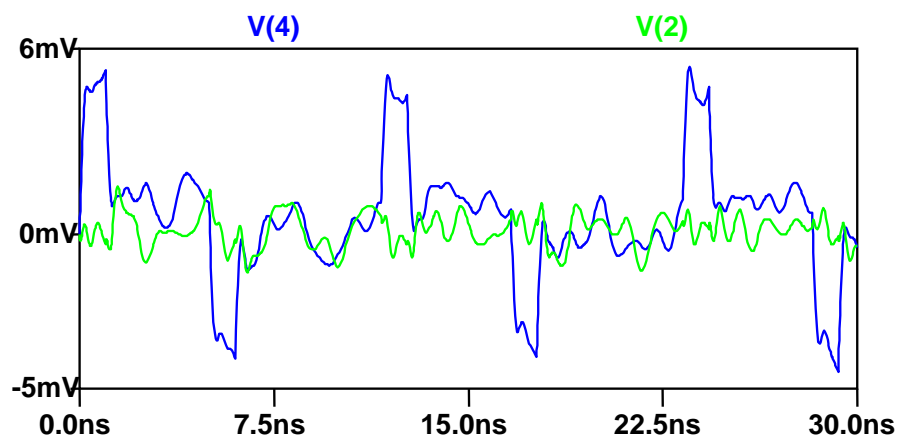
A pulse is applied to port 4



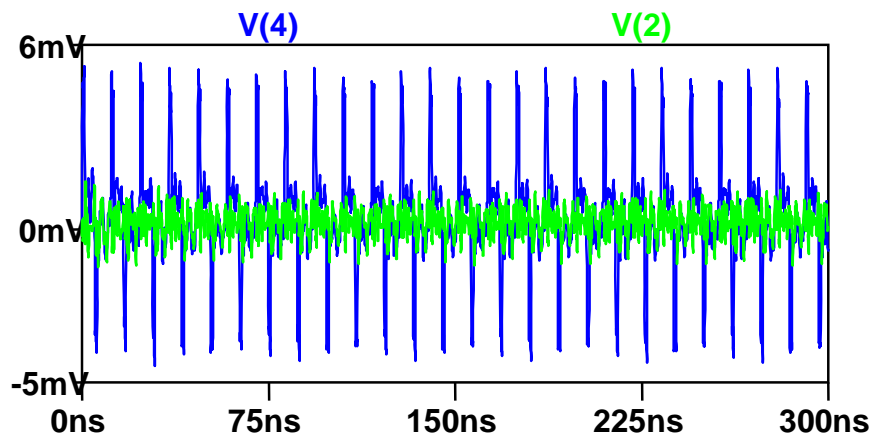
S. Grivet-Talocia, "On Driving Non-passive Macromodels to Instability", *International Journal of Circuit Theory and Applications*, vol. 37, n. 8, pp. 863-886, October, 2009



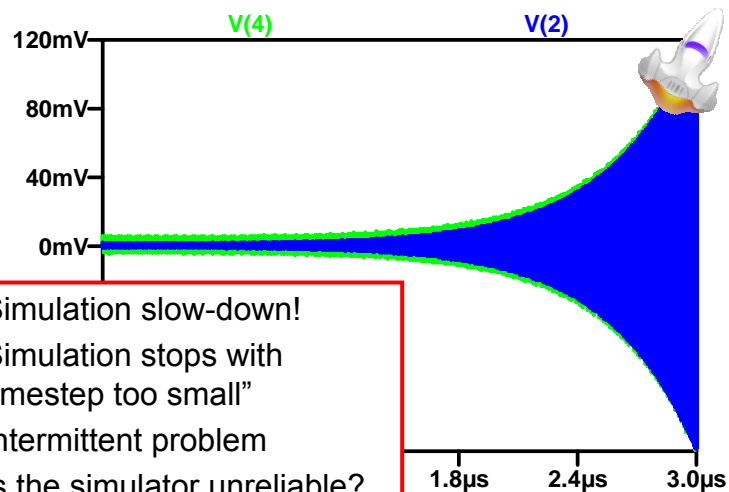
Transient simulation results



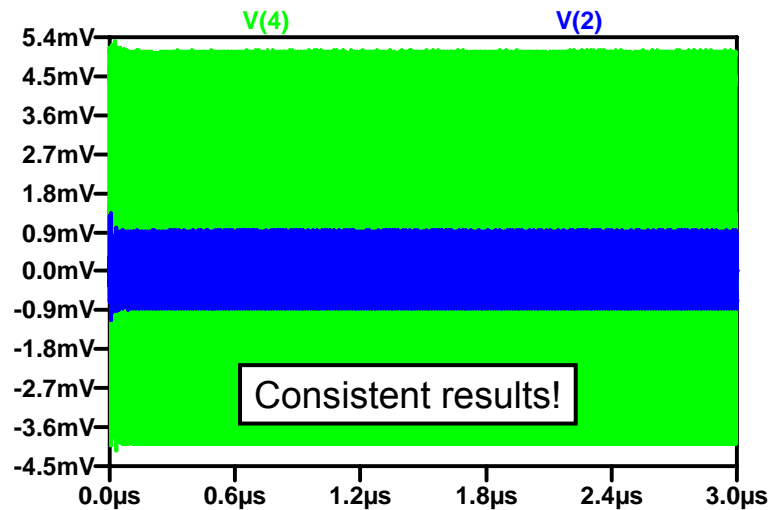
Transient simulation results



Transient simulation results



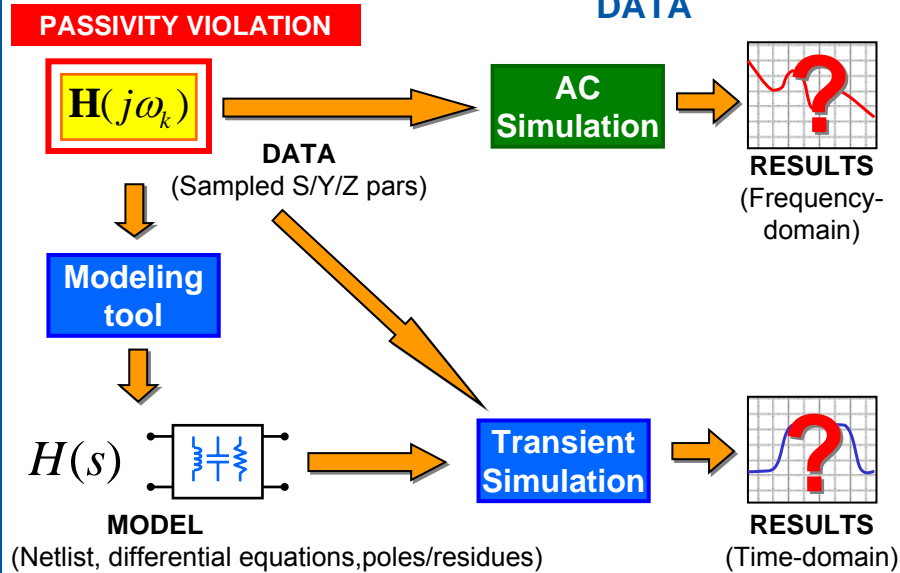
If model passivity is instead enforced...



Best practices

- Use passive models for passive components!
- If a given model violates passivity, compensate the violation with one of the well-established methods (see references at the end):
 - convex optimization
 - Hamiltonian matrices
 - linear and quadratic programming
- If violations are large, compensate violations with discretion! Or take the safe way: redo the model

Passivity violation in the DATA



Passivity in frequency domain

Passivity conditions (frequency domain):

- 1) $\mathbf{H}(-j\omega) = \mathbf{H}^*(j\omega)$
- 2) $\mathbf{H}^H(j\omega)\mathbf{H}(j\omega) \leq \mathbf{I}$
- 3) Check if $\mathbf{H}(j\omega)$ is causal
(i.e. check dispersion relations)

$$\mathbf{H}(j\omega)$$

- Mind the third condition!
- Allow for a complete passivity check for tabulated data

P. Triverio, S. Grivet-Talocia, "Robust Causality Characterization via Generalized Dispersion Relations", *IEEE Trans. on Advanced Packaging*, vol.31, n.3, August, 2008

Passivity violations in FREQUENCY DATA



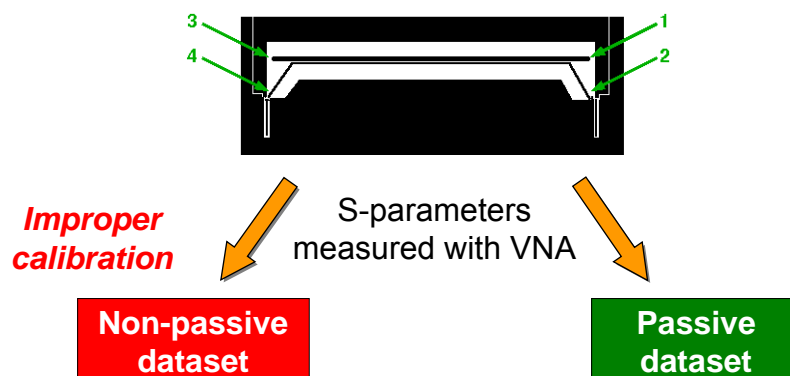
HOW can passivity violations arise?

- **Numerical simulation:** poor meshing, bad models or assumptions on material properties, inaccurate solver, human mistakes
- **Measurement:** Improper VNA calibration/de-embedding, human mistake, noise
- What happens if starting frequency data are not passive?

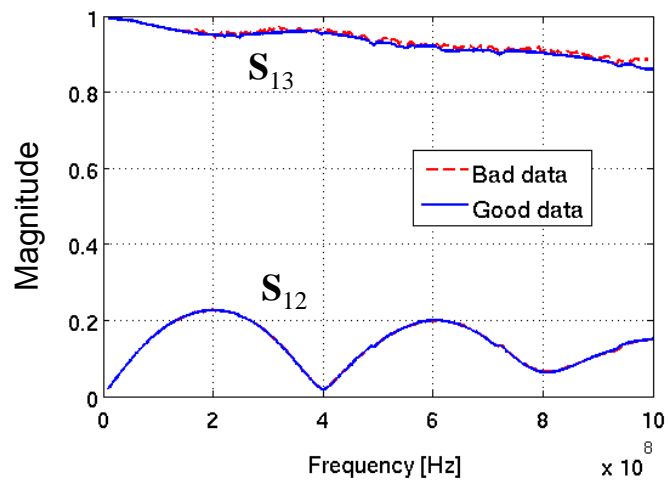


Example: passive vs non-passive data

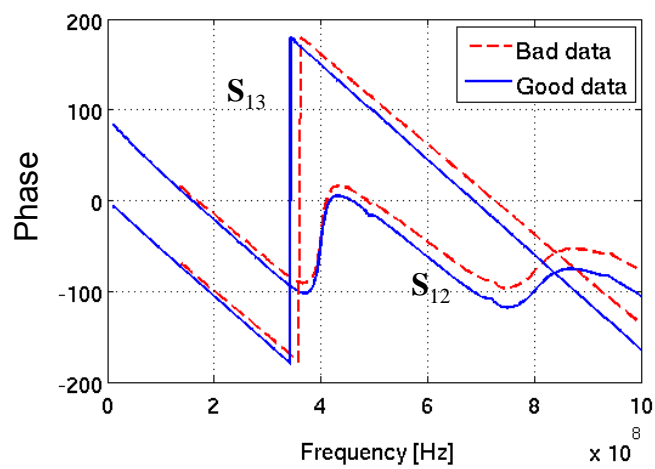
- For this PCB coupled lines, two different measurements were performed



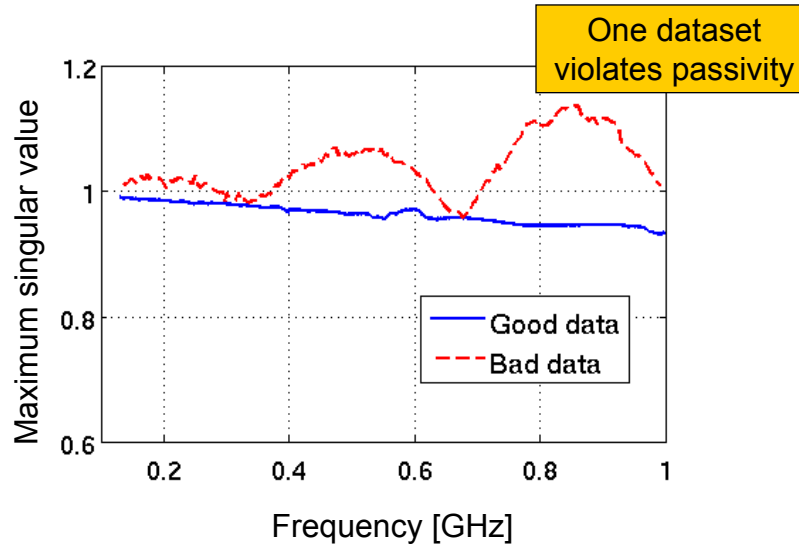
Example: passive vs non-passive data



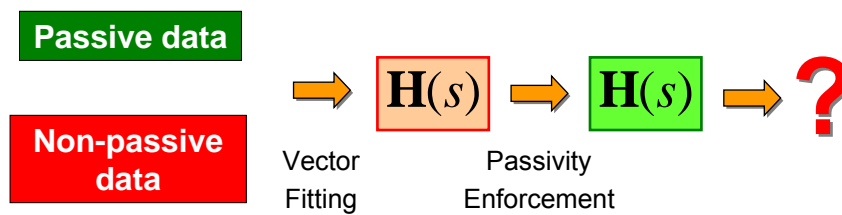
Example: passive vs non-passive data



Example: passive vs non-passive data



Example: passive vs non-passive data



Example: passive vs non-passive data

Non-passive data

Passive data

Vector Fitting model order			
6			
12			
18			

Example: passive vs non-passive data

Non-passive data

Passive data

Vector Fitting model order	Passivity not enforced		
6	0.280		
12	0.020		
18	0.017		



Model is not
passive!

Example: passive vs non-passive data

Non-passive data

Passive data

Vector Fitting model order	Passivity not enforced	Passivity enforced	
6	0.280	0.23	
12	0.020	0.11	
18	0.017	0.13	



Model is not
passive!



Model not
accurate!

Example: passive vs non-passive data

Non-passive data

Passive data

Vector Fitting model order	Passivity not enforced	Passivity enforced	Passivity enforced
6	0.280	0.23	0.240
12	0.020	0.11	0.020
18	0.017	0.13	0.012



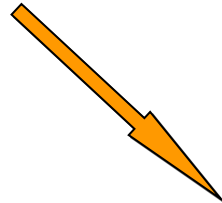
Passive &
accurate!

Passivity violation in the DATA

PASSIVITY VIOLATION

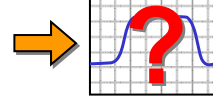
$$\mathbf{H}(j\omega_k)$$

DATA
(Sampled S/Y/Z pars)



Transient
Simulation

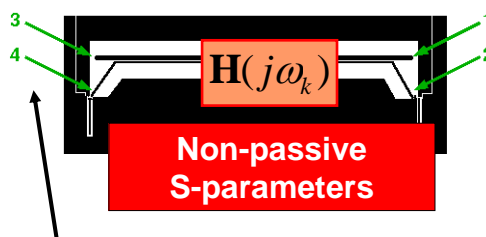
Convolution-based



RESULTS
(Time-domain)

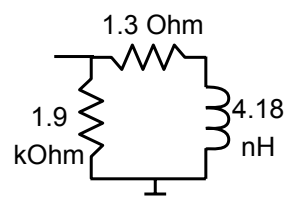
Convolution simulation setup

- The coupled lines (represented by the Touchstone file) are connected to a destabilizing load



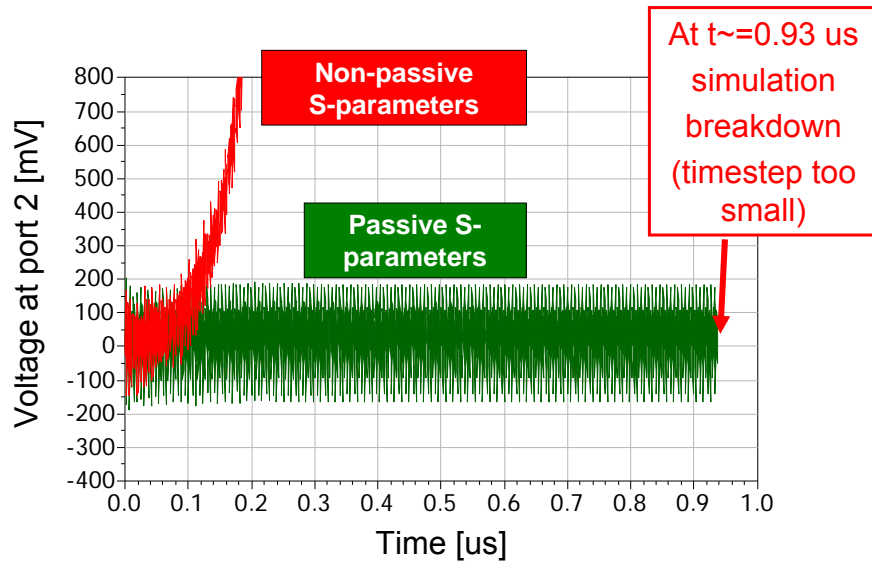
A 1mA current pulse is applied to port 4

All ports loaded with

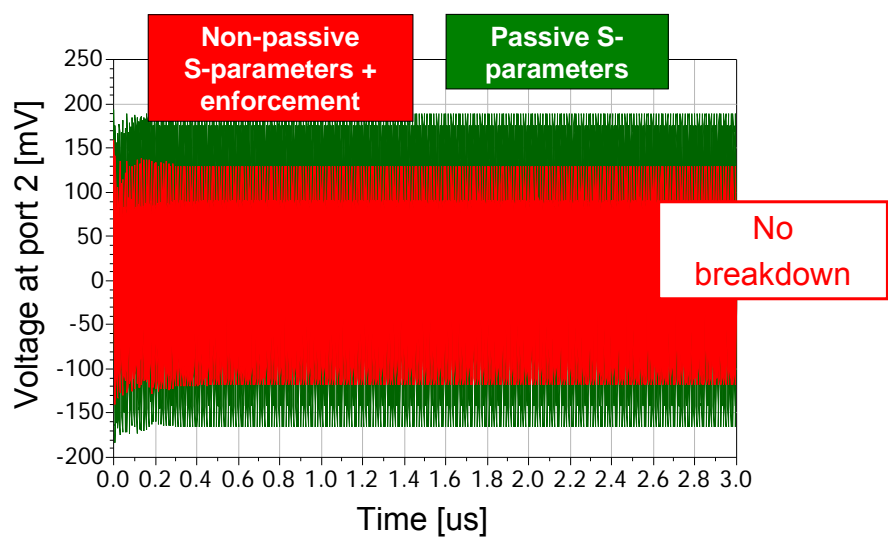


The same analysis is repeated with the **passive S-parameters**

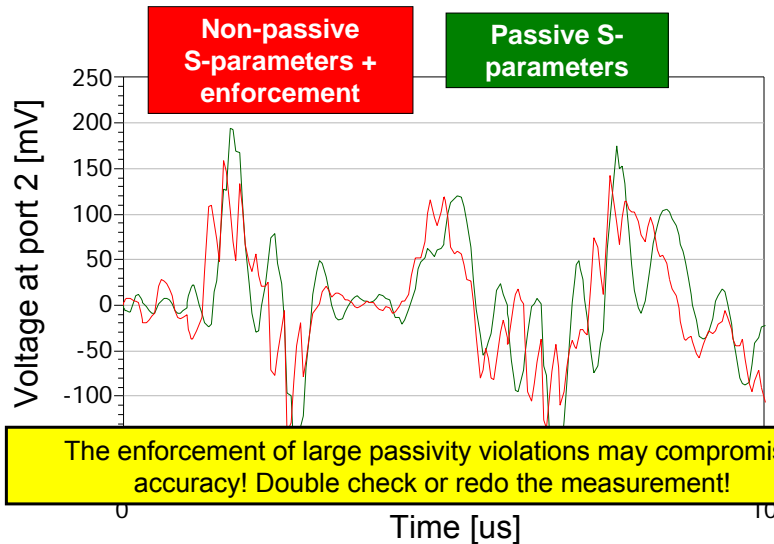
Convolution simulation



Convolution simulation (passivity enforcement ON)



Convolution simulation (passivity enforcement ON)



Best practices

- If you have a dataset with significant passivity violations, you will have to renounce to either:
 - accuracy (will you trust your results?)
 - model passivity (simulations may diverge!)
- Promptly scan your measured/simulated data for passivity violations! For an algorithm, see [1]
- And reject “bad” datasets!

[1] P. Triverio, S. Grivet-Talocia, "Robust Causality Characterization via Generalized Dispersion Relations", *IEEE Trans. on Advanced Packaging*, vol.31, n.3, August, 2008

Conclusion

- Comprehensive overview of **causality, stability & passivity** and their interrelations
- Impact of physical consistency violations on modeling and simulation tasks
 - models with violations → **divergent simulations!**
 - data with violations → either **inaccurate models** or **unstable simulations**
- When consistency is preserved → **Accuracy, speed and reliability** of CAD tools is maximized!



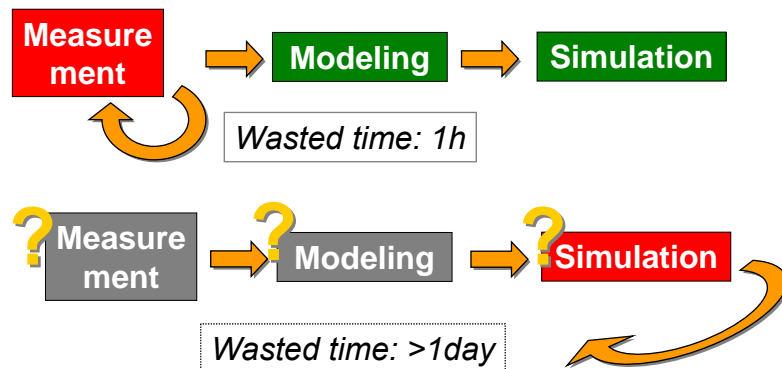
Conclusion

- Being aware of the importance of physical consistency can improve the design workflow significantly!



Conclusion

- Problems can be fixed right away!
- Physical consistency checks greatly help to identify the real source of the problems!



Thank you!



Bibliography: high-speed interconnects

- C. Paul, *Analysis of Multiconductor Transmission Lines*. John Wiley & Sons, Inc. New York, NY, USA, 1994.
- R. Achar and M. Nakhla, "Simulation of high-speed interconnects," *Proceedings of the IEEE*, vol. 89, no. 5, pp. 693–728, 2001.
- M. Celik, N. Pileggi, and A. Odabasioglu, *IC interconnect analysis*. Kluwer Academic Publishers, 2002.



Bibliography: Vector Fitting

- B. Gustavsen and A. Semlyen, "Rational approximation of frequency domain responses by Vector Fitting," *IEEE Trans. Power Del.*, vol. 14, no. 3, pp. 1052–1061, July 1999
- "The VF Web Site" <http://www.energy.sintef.no/produkt/VECTFIT/index.asp>
- D. Deschrijver, M. Mrozowski, T. Dhaene, and D. De Zutter, "Macromodeling of Multiport Systems Using a Fast Implementation of the Vector Fitting Method," *IEEE Microwave and Wireless Components Letters*, vol. 18, no. 6, pp. 383–385, 2008.
- S. Grivet-Talocia, "Package Macromodeling via Time-Domain Vector Fitting", *IEEE Microwave and Wireless Components Letters*, pp. 472-474, vol. 13, n. 11, Nov. 2003
- Y.S. Mekonnen, J.E. Schutt-Aine, "Fast Macromodeling Technique of Sampled Time/Frequency Data Using z-domain Vector-Fitting Method", *EPEP 2007*, Atlanta, GA, Oct 29-31, 2007, pp. 47 – 50
- B. Nouri, R. Achar, M. Nakhla, D. Saraswat, "z-Domain Orthonormal Vector Fitting for Macromodeling High-Speed Modules Characterized by Tabulated Data," *IEEE Workshop on Signal Propagation on Interconnects*, Avignon, France, May 2008.
- B. Gustavsen and C. Heitz, "Modal Vector Fitting: A Tool for Generating Rational Models of High Accuracy with Arbitrary Terminal Conditions", *IEEE Trans. Advanced Packaging*, vol. 31, no. 4, pp. 664-672, November 2008



Bibliography: passivity enforcement

- C. P. Coelho, J. Phillips, and L. M. Silveira, "A convex programming approach for generating guaranteed passive approximations to tabulated frequency-data," *IEEE Trans. Computed-Aided Design Integrated Circuits Syst.*, vol. 23, no. 2, Feb. 2004.
- B. Gustavsen, A. Semlyen, "Enforcing passivity for admittance matrices approximated by rational functions," *IEEE Trans. Power Syst.*, vol. 16, no. 1, pp. 97–104, Mar. 2001.
- D. Saraswat, R. Achar, and M. Nakhla, "A fast algorithm and practical considerations for passive macromodeling of measured/simulated data," *IEEE Trans. Components, Packaging and Manufacturing Technol.*, vol. 27, pp. 57–70, Feb. 2004.
- S. Grivet-Talocia, "Passivity enforcement via perturbation of Hamiltonian matrices," *IEEE Trans. Circuits Syst.—I*, vol. 51, no. 9, pp. 1755–1769, Sep. 2004.
- S. Grivet-Talocia, A. Ubolli, "A Comparative Study of Passivity Enforcement Schemes for Linear Lumped Macromodels", *IEEE Transactions on Advanced Packaging*, vol.31, n.4, pp. 673-683, November, 2008
- T. Dhaene, D. Deschrijver, N. Stevens, "Efficient Algorithm for Passivity Enforcement of S-parameter Based Macromodels", *IEEE Transactions on Microwave Theory and Techniques*, Vol. 57, No. 2, pp. 415-420, February 2009.



Bibliography: transmission lines macromodeling

- S. Grivet-Talocia, H. Huang, A. Ruehli, F. Canavero, and I. Elfadel, "Transient Analysis of Lossy Transmission Lines: An Efficient Approach Based on the Method of Characteristics," *IEEE Trans. Adv. Packag.*, vol. 27, no. 1, pp. 45–56, 2004.
- N. Nakhla, A. Dounavis, R. Achar, and M. Nakhla, "DEPACT: delay extraction based passive compact transmission-line macromodeling algorithm," *IEEE Trans. Adv. Packag.*, vol. 28, no. 1, pp. 13–23, 2005.
- E. Gad, C. Chen, M. Nakhla, and R. Achar, "Passivity verification in delay-based macromodels of electrical interconnects," *IEEE Trans. Circuits Syst. I*, vol. 52, no. 10, pp. 2173–2187, Oct. 2005.
- A. Chineza, S. Grivet-Talocia, "Perturbation Schemes for Passivity Enforcement of Delay-Based Transmission Line Macromodels", *IEEE Transactions on Advanced Packaging*, vol.31, n.3, pp. 568-578, August, 2008



Bibliography: delay-based macromodeling

- A. Chinae, P. Triverio, S. Grivet-Talocia, "Delay-Based Macromodeling of Long Interconnects from Frequency-Domain Terminal Responses", *IEEE Transactions on Advanced Packaging*, Vol. 33, n.1, pp. 246-256, February, 2010
- A. Charest, D. Saraswat, M. Nakhla, R. Achar, and N. Soveiko, "Compact Macromodeling of High-Speed Circuits via Delayed Rational Functions," *IEEE Microwave and Wireless Components Letters*, vol. 17, no. 12, pp. 828-830, 2007.
- P. Triverio, S. Grivet-Talocia, A. Chinae, "Identification of highly efficient delay-rational macromodels of long interconnects from tabulated frequency data", *IEEE Transactions on Microwave Theory and Techniques*, Vol. 58, n. 3, pp. 566-577, 2010
- A. Charest, M. Nakhla, R. Achar, D. Saraswat, N. Soveiko, I. Erdin, "Time Domain Delay Extraction-Based Macromodeling Algorithm for Long-Delay Networks", *IEEE Transactions on Advanced Packaging*, vol. 33, n. 1, pp. 219 – 235, Feb 2010.
- A. Charest, M. Nakhla, R. Achar, C. Chen, "Passivity verification and enforcement of delayed rational function macromodels from networks characterized by tabulated data," in *IEEE Workshop on Signal Propagation on Interconnects*, 2009. SPI'09, pp. 1-4, May 12-15, 2009.



Bibliography: multivariate macromodeling

- P. Triverio, M. Nakhla, S. Grivet-Talocia, "Parametric Macromodeling of Multiport Networks from Tabulated Data" , *IEEE 16th Topical Meeting on Electrical Performance of Electronic Packaging (EPEP 2007)*, Atlanta (GA), USA, pp. 51-54, October 29-31, 2007
- D. Deschrijver, T. Dhaene, D. De Zutter, "Robust Parametric Macromodeling using Multivariate Orthonormal Vector Fitting", *IEEE Transactions on Microwave Theory and Techniques*, Vol. 56, No. 7, pp. 1661-1667, July 2008.
- P. Triverio, S. Grivet-Talocia, M.S. Nakhla, "A Parameterized Macromodeling Strategy with Uniform Stability Test" , *IEEE Transactions on Advanced Packaging*, Vol. 32, n.1, pp. 205-215, February, 2009
- F. Ferranti, L. Knockaert, T. Dhaene, "Parameterized S-parameter Based Macromodeling with Guaranteed Passivity", *IEEE Microwave and Wireless Components Letters*, Vol. 19, No. 10, pp. 608-610, October 2009.



Bibliography: stability, passivity and causality

- P. Triverio, S. Grivet-Talocia, M. S. Nakhla, F. C. Canavero, R. Achar, "Stability, causality, and passivity in electrical interconnect models," *IEEE Transactions on Advanced Packaging*, vol. 30, n. 4, Nov. 2007, pp. 795 – 808
- P. Triverio, S. Grivet-Talocia, "Robust Causality Characterization via Generalized Dispersion Relations", *IEEE Transactions on Advanced Packaging*, vol.31, n.3, pp. 579-593, August, 2008
- M. R. Wohlers, "Lumped and Distributed Passive Networks", New York: Academic, 1969.
- A. V. Oppenheim and A. S. Willsky, "Signals and Systems", Englewood Cliffs, NJ: Prentice–Hall, 1983.
- S. Grivet-Talocia, "On Driving Non-passive Macromodels to Instability" , *International Journal of Circuit Theory and Applications*, vol. 37, n. 8, pp. 863-886, October, 2009